Termite Spatial Correlation Based PSO (TSC-PSO)

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Outline



- ress.com Introduction to Optimization
- Particle Swarm Optimization (PSO) Algorithm
- Variants in PSO
- Ant colony Optimization
- Inspiration Termites
- Development of Algorithm Parameter Study Tests



Optimization is Everywhere



- The more we know about something, the more we see where optimization can be applied.
- Some personal decision making
 - Finding fastest route home or class
 - Optimal allocation of time for home work
 - Optimal budgeting





Mathematical Formulation of Optimization **Problems** .dpress.com minimize the objective function $\min f(x), x = (x_1, x_2, \dots, x_n)$ 281.MOR subject to constraints https://draiestexample $C_i(x) \ge 0$ $c_i(x) = 0$ $\min\left[\left(x_{1}-2\right)^{2}+\left(x_{2}-1\right)^{2}\right]$ subject: $x_1^2 - x_2^2 \le 0$ $x_1 + x_2 \le 2$

Linear Non-linear Classification of Optimization Methods



Figure 1: bird flocking and Fish schooling



The basic idea



ttps://

- Each particle is moving (can't search otherwise!), and hence has a velocity.
- Each particle remembers the position it was in where it had its best result so far (its personal best)
- But this would not be much good on its own; particles need help in figuring out where to search.



The basic idea



- The particles in the swarm *co-operate*. They exchange information about what they' ve discovered in the places they have visited
- The co-operation need only be very simple. In basic PSO (which is pretty good!) it is like this:
 - A particle has a *neighbourhood* associated with it.
 - A particle knows the fitnesses of those in its neighbourhood, and uses the *position* of the one with best fitness.
 - This position is simply used to adjust the particle's velocity



Neighborhoods

























Particle Swarm Optimisation Swarm search



Velocity calculation

city calculation

$$v_{id(t)} = \omega v_{id(t-1)} + c_1 \times rand() \times (p_{id} - x_{id}) + c_2 \times Rand() \times (p_{gd} - x_{id})$$

$$x_{id(t)} = x_{id(t-1)} + v_{id(t)}$$

Position update $x_{id(t)} = x_{id(t-1)} + v_{id(t)}$ x_{id} – current value of the dimension "d" of the dividual "i" v_{id} – current velocity of the dimension "d" of the individual "i". P_{id} – optimal value of the dimension "d" of the individual "i" so far. P_{ad} – current optimal value of the dimension "d" of the swarm. $c_1, c_2 - acceleration coefficients.$ ω - inertia weight factor





- press.com There are a number of related issues concerning PSO:
 - Controlling velocities (determining the best value for Vmax),
 - Swarm Size,

 - Inertia weight factor, Multi
 Robust Settings for (C1 and C2),







- 1. Initialise particles in the search space at random.
- 2. Assign random initial velocities for each particle.
- 3. Evaluate the fitness of each particle according a user defined objective function.
- 4. Calculate the new velocities for each particle.
- 5. Move the particles.
- 6. Repeat steps 3 to 5 until a predefined stopping criterion is satisfied.



Some Comments on C_1 C_2

- c1 = c2 = 0?
- c1 > 0, c2 = 0:

cognition-only model

• c1 = 0, c2 > 0:

social-only model

• c1 = c2 > 0:

particles are attracted towards the average of yi and ^yi

c2 > c1:
 more beneficial for unimodal problems

- c1 < c2: more beneficial for multimodal problems
- **bow** c1 and c2:
- smooth particle trajectories
- High c1 and c2:

more acceleration, abrupt movements

- Adaptive acceleration coefficients
- c1(t) = (c1,min c1,max)t/nt + c1,max
- c2(t) = (c2,max c2,min) t/nt + c2,min

Natural behavior of ant



Ant Algorithms – (P.Koumoutsakos – based on notes L. Gamberdella (www.idsia.ch)





Termites



- Similar to ants, termites belong to a category of eusocial insects that work as decentralized entities in their group.
- Termites are relatively simple insects of small size with a small number of neurons within them.
- This limits their ability to perform complex tasks at the individual level.
- On the other hand, a termite colony acts as an intelligent entity exhibiting a high level of self-organization and perform highly complex tasks.
- They exhibit relatively simple rules at the individual level to perform complex tasks at the group level without any form of centralized control.
- Their colonies can range from few hundred to few million in size.





- A typical termite colony consists of nymphs, workers, soldiers and reproductive individuals within it.
- To design any swarm intelligence inspired algorithm it is necessary to understand whether the given group replicate features of self-organization or not.
- In any decentralized systems, all the individual entities work on the basis of local information to achieve a common goal.
- Self-organization is a process in which with the help of some local interactions between the lower system of entities some coordination occurs in the working of the group.
- This process occurs with some sort of initial randomness and is not controlled by any external/central authority.
- This overall process takes place in a decentralized manner such that individual entities work on the basis of local information.





- Being a decentralized group, termite colony use a mechanism called stigmergy that is a kind of self-organization in which individuals in a group try to coordinate by indirect communication.
- Similar to ants, termite agents' use indirect communication by sensing and modifying the local environment.
- Termite workers build a nest by following a set of simple decentralized rules.
- Each worker takes a mud-ball from the environment and adds a small amount of pheromone to it.
- Then this mud-ball is initially placed probabilistically at a random position on the ground.
- But the probability of depositing a mud-ball at a particular place is increased with increase in the concentration of pheromone at that location.
- By mud-ball placing columns of nest gets formed. This process of nest building is similar to trail recruitment process as replicated within ant colonies.





- Various features exhibited by a self-organized system are
- **Positive and negative feedback**: These Information are taken from the output and applied back to the input of the system. Positive feedback tries to take system towards more stable state.
- Fluctuations: Fluctuations includes those process that introduces randomness into the system. For proper working of any self-organized system, these fluctuations are important as they help system to avoid stagnation and helps to maintain a proper balance between exploration and exploitation.
- **Multiple interactions**: This provides a mechanism for the system to have a combined intelligence by the process of learning through the information of individuals in the society.



Patterns









• Cornitermes cumulans termite workers are correlated to a certain extent. The individual steps in the termite walking were dependent on the previous steps with dependency getting decreased along the trajectory. For analyzing the correlation among the successive steps they used a correlation function (C.F.).





- The termite walking pattern was found to have long range correlations decaying as power laws.
- This step correlation exhibited by the termite workers became the inspiration for our work.
- The proposed algorithm tries to incorporate this step correlation by using greed based correlation multiplication factor selection.
- The algorithm does so by selecting a comparatively higher factor for the favorable regions.
- This process of selection of proper factor acts as a feedback to the system.
- Further evolutionary features were added to the algorithm to help the algorithm to avoid stagnation.





- Each individual in the swarm is called agent. Each agent has seven attributes/properties associated with it: -
- Position: It denotes the present position of the agent within the sample space
- Fitness: represent fitness or objective function value of the agent at
- Velocity: It denotes the amount of movement that the individual agent would undergo in the present iteration
- Best position & Fitness: It denotes the best position and fitness (in terms of fitness) that has been found by the agent so far.
- **Best fitness**: Represented by *pbestfit*_i, it denotes the fitness or objective function value of the agent ' i' at *pbest*_i.
- Past velocities Past velocities of the agent.
- Correlation coefficient: It represents the weight of particular past velocity in the present velocity.

Phase -1: Attribute Update Phase



- This phase involves updating various attributes like fitness, past velocities, correlation coefficients, best position and best fitness of each agent
- At first fitness or objective function value of the agent at the current position is evaluated. This is followed by updating past velocity and correlation coefficient matrices
- If the present fitness value is better than the previous fitness of the agent than the CC(i, 1) is updated to a higher value (CC_{high})
- This helps the agent to move more in the direction in which it finds better fitness values as compared to those directions in which it's fitness decreases

Phase – 2: Replacement and Mutation Phase



- Agents with worst fitness are killed and replaced by new agents.
- R bad performing agents are killed and replaced with new agents by initializing them according to attributes of surviving agents in the swarm.
- This is followed by mutating one of the randomly selected dimensions of each new agent by using mutation equation

$$x_{i,j} = x_{i,j} + r_3 * [ub_j - lb_j]/2$$

• Although this phase can result in slightly reduced convergence rate it helps the algorithm to avoid stagnation condition.



Phase – 3: Swarm Update Phase



- This phase involves updating each agent's velocity and position in the search space so as to be used in the next iteration.
- Velocity update equation:-

 $v_{i} = \sum_{t=1}^{t_{max}} [CC(i, t)*vpast_{i}^{t}] + c_{1}*r_{1}*(pbest_{i} - x_{i}) + c_{2}*r_{2}*(gbest - x_{i})$

• The algorithm makes use of past tmax velocities in a greedy manner to formulate a correlation function as a replacement for weighted (inertia weights) velocity.



Impact of Hyper Parameters CCDF







C1-C2 Tuning curves







(e) Ackley function, (f) Kennedy multimodal function generator (M=1 peaks),(g) Kennedy multimodal function generator (M=10 peaks),

(h) Kennedy multimodal function generator (M=100 peaks).



Benchmark Functions



Function	D	Range	f _{min}	<u> </u>
Elliptic	30	[-100,100]	05	U
Sphere	30	[-100, 100]	S. Contractions	U
Greiwank	30	[-600,600]	0	Μ
Rastrigin	30	[-5.12,5.12]	0	М
Rosenbrock	30	[-5,10]	0	U
Schwefel 1.2	30	[-100,100]	0	U
Ackley	30	[-32,82]	0	М
Step	30	[-199,100]	0	U
Shifted Elliptic	30	100,100]	0	U
Shifted Ackley	30	[-32,32]	0	Μ
Beale	2	[-4.5,4.5]	0	U
Six Hump Camel Back	2	[-5,5]	-1.0316	Μ
Hartmann 3D	d'	[0,1]	-3.8628	Μ
Hartmann 6D	6	[0,1]	-3.3224	M
Easom	2	[-100, 100]	-1	U
Goldstein	2	[-2,2]	3	Μ
Schwefel 2.22	30	[-10,10]	0	U
Schwefel 2.21	30	[-100, 100]	0	U
Schwefel	30	[-500,500]	0	Μ
Noise	30	[-1.28, 1.28]	0	U
Penalised1	30	[-50,50]	0	Μ
Penalised2	30	[-50,50]	0	M
Shifted Rotated	30	[-100, 100]	0	Μ
Rotated Greiwank	30	[-600,600]	0	Μ
Rotated	30	[-32,32]	0	Μ
Composition function 1	10	[-5,5]	0	М
Composition function 2	10	[-5.5]	0	M

Comparison with GWO , PSO , GSA,DE, ABC and FEP



F		TSC-PSO	GWO	P50	GSA	DE	ABC	FEP
fl	Meen	1.76E=108	4.45E-24	2.33E=04	4.57E-15	7.87E-13	4,60E-09	2.48E-04
	StD	4.65E-109	2.73E-24	1.04E=04	2.78E-15	6.11E-13	7.80E-10	1.98E-04
	t(h)		-11.63(1)	-15.93(1)	-11.72(1)	-9.2(1)	-42.07(1)	-8.92(1)
f2	Meen	5.07E=128	7.46E-28	1.48E=04	2.94E-16	8.7.E-4	7.32E-16	6.16E=04
	StD	1.71E=128	5.42E-28	4.38E=05	2.56E-16	2645-14	2.95E-16	3.85E-04
	r-test:t(h)		-9.82(1)	-24.17(1)	-8.2(1)	-21)89(1)	-17.7(1)	-11.43(1)
13	Meen	1.27E-02	4.13E-03	7.88E-03	4.45E+01	0.00E+00	3.35E-13	1.59E-02
	StD	8.15E=03	3.13E-03	6.41E=03	3.77E+02	0.00E+00	1.74E-13	7.41E=03
	t velue		6.97(1)	3.29(1)	-8.4461	11.09(1)	11.09(1)	-2.1(1)
f 4	Meen	1.28E=11	2.83E-01	6.93E+01	3,052+01	5.92E+01	1.35E-03	5.94E-02
	StD	2.14E-12	1.16E-01	2.54E+01	6.82E+00	3.71E+01	8.49E=04	1.18E-02
	t velue		-17.44(1)	-19.49(1)	32.05(1)	-11.41(1)	-11.37(1)	-35.92(1)
f5	Meen	8.45E=14	2.53E+01	1.50E+02	7.15E+01	0.00E+00	8.70E-02	4.54E+00
	StD	4.09E-14	5.71E+00	9.852481	6.12E+01	0.00E+00	6.63E-02	8.87E-01
	t velue		-31.65(1)	-10.9(5)	-8.34(1)	14.75(1)	-9.38(1)	-36.58(1)
f6	Meen	2.24E=122	3.59E-06	7.94E+01	9.98E+02	7.15E-11	3.84E-12	1.70E-02
	StD	6.83E=123	9.23E-07	S.06E+01	6.50E+02	2.85E-11	2.12E-12	5.22E-03
	t velue		-27.77(1)	-18.27(1)	-10.96(1)	-17.92(1)	-12.93(1)	-23.24(1)
17	Meen	9.87E=13	1.93E 18 1	4.65E-01	5.26E-02	1.16E-07	1.73E-09	2.63E-02
	StD	2.62E=13	5.363-14	2.06E=01	2.67E-02	8.14E-08	7.76E=10	1.73E=02
	t velue		(22)(i)	-16.12(1)	-14.1(1)	-10.14(1)	-15.91(1)	-10.83(1)
18	Meen	0.00E+00	1.25E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
	StD	0.00E+00	6.44E-01	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
	t velue		-13.88(1)	0(0)	0(0)	0(0)	0(0)	0(0)
19	Meen	0.00E+08	4.05E-27	8.22E-06	7.67E-21	7.51E-18	5.03E-15	6.27E=14
	StD	0.0000	1.73E=27	6.10E-06	6.75E-21	2.77E-18	2.49E=15	3.08E-14
	t velue	0	-16.7(1)	-9.62(1)	-8.12(1)	-19.34(1)	-14.43(1)	-14.54(1)
f10	Mean	1.99E-14	2.98E+01	1.56E+01	1.55E+01	2.87E-05	1.12E-04	2.67E+01
	510	1.37E-14	2.24E+01	1.32E+01	8.27E+00	1.58E-05	6.24E-05	1.97E+01
	t velue		-9.52(1)	-8.4(1)	-13.37(1)	-12.97(1)	-12.8(1)	-9.66(1)
fII	Meen	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
	StD	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
	t velue		0(0)	0(0)	0(0)	0(0)	0(0)	0(0)
f12	Meen	-1.03E+00	-1.03E+00	-1.03E+00	-1.03E+00	-1.03E+00	-1.03E+00	=1.03E+00
	StD	0.00E+00	0.00E+00	5.71E-15	4.48E-16	2.71E-13	3.46E=04	8.91E-08
	t velue		0(0)	0(0)	0(0)	0(0)	-21.78(1)	0(0)

Comparison with GWO , PSO , GSA,DE, ABC and FEP



<i>.</i>								>
F		TSC-PSO	GWO	PSO	GSA	DE	ABC	FEP
f13	Meen	-3.86E+00	-3.86E+00	-3.86E+00	-3.86E+00	-3.86E+00	-3.552+00	-3.86E+00
	StD	0.00E+00	4.14E+05	3.58E+14	7.11E=14	1.71E-14	0.0714	8.40E=06
	t velue		0(0)	0(0)	0(0)	0(0)	-8.57(1)	0(0)
f14	Meen	-3.29E+00	-3.29E+00	-3.27E+00	-3.32E+00	-3.295+0	-3.32E+00	-3.27E+00
	StD	0.057582013	0.001221	0.060516	0.023081	0.045455	2.25E-06	0.059
	t velue		0(0)	-1.04(0)	2.17(1)		2.77(1)	-0.91(0)
f15	Meen	-1.00E+00	-1.00E+00	-1.00E+00	-1.00E+00	-1.00E+00	-1.00E+00	-1.00E+00
	StD	0.00E+00	0.00E+00	2.17E-14	0.00E+00	616E-15	3.64E-07	0.00E+00
	t velue		0(0)	0(0)	0(0)	0(0)	0(0)	0(0)
f16	Meen	3.00E+00	3.00E+00	3.00E+00	3.00E+00	3.00E+00	3.09E+00	3.02E+00
	StD	0.00E+00	3.12E-06	1.33E-15	4.17E-15	2.00E-15	1.14E-01	9.87E-02
	t velue		-17.68(1)	0(0)	000	0(0)	-9.7(1)	-75.12(1)
f17	Mean	1.37E=37	8.21E-17	4.13E=02	5.50E-02	1.65E-09	8.09E-11	9.70E-03
	StD	9.18E-38	3.53E=17	2.22E-02	L47E-02	1.22E-09	1.92E-11	6.44E-03
	t velue		-16.62	-13.31(1)	-26.73(1)	-9.71(1)	-30.13(1)	-10.75(1)
f18	Meen	4.70E=11	6.50E-07	1.255490	8.37E+00	0.00E+00	1.14E+01	3.03E-01
	StD	3.21E=11	3.59E-07	2.51B-01	4.05E+00	0.00E+00	9.63E+00	2.17E-01
	t velue		-12.95(1)		-14.78(1)	10.46(1)	-8.47(1)	-10.01(1)
f19	Meen	0.00E+00	9.52E+03	24E+04	8.85E+03	2.64E+03	1.09E+02	1.28E+01
	StD	0.00E+00	7.24E+03	6.41E+03	5.14E+08	1.70E+03	2.06E+01	7.96E+00
	t velue		-9.39(1)	-13.81(1)	-12.29(1)	-11.06(1)	-37.88(1)	-11.44(1)
f20	Meen	1.94E=03	2.565-03	1.35E-01	1.08E=01	4.69E=03	1.38E-01	1.44E-01
	StD	1.00E-03	\$ 48E-14	1.13E=01	2.34E=02	3.61E=03	9.27E-02	3.56E-02
	t velue		-1 95(1)	-8.35(1)	-32.35(1)	-5.25(1)	-10.49(1)	-28.52(1)
f21	Meen	1.79E-32	7.68E-02	1.23E-02	2.74E+00	8.75E-15	4.37E-14	1.07E-05
	StD	8.69E-33	4.24E-02	6.55E=03	6.92E=01	1.77E-15	1.38E-14	6.18E-06
	t velue	YX.	-12.95(1)	-13.42(1)	-28.24(1)	-35.33(1)	-22.59(1)	-12.38(1)
f22	Meen	162E-30	6.51E-01	5.38E-03	1.03E+01	5.38E-14	6.63E-15	1.79E-04
	StD	1.186-30	5.26E-01	4.31E=03	4.83E+00	1.92E-14	4.91E-15	1.28E-04
	t velue	Ŧ	-8.85(1)	-8.93(1)	-15.23(1)	-20.04(1)	-9.64(1)	-10(1)
f26	Meen	1.25E+02	1.36E+02	3.23E+02	1.93E+02	3.24E+02	3.30E+02	2.72E+02
	StD	8.25E+01	8.91E+01	2.69E+02	4.43E+01	2.81E+02	2.08E+02	1.25E+02
	t velue		-0.64(0)	-5(1)	-5.12(1)	-4.86(1)	-6.53(1)	-6.96(1)
f27	Meen	1.08E+02	1.14E+02	8.37E+01	2.00E+02	1.19E+01	1.52E+02	1.80E+02
	StD	2.18E+01	4.52E+01	5.04E+01	1.24E+02	3.45E+00	1.10E+02	3.64E+01
	t velue		-0.9(0)	3.16(1)	-5.19(1)	31.07(1)	-2.82(1)	-12.12(1)

Shepiro-Wilk test for TSC-PSO, GWO [5], PSO [23], GSA [15], DE [13], ABC [26] and FEP [14] samples.						Wilcox	on test again	et GWO [5], 1	PSO [23], GS	A [15], DE [1:	3], ABC [26]	and FEP [14].		
F	TSC-	GWO	PSO	GSA	DE	ABC	FEP	F	GWO	PSO	GSA	DE	ABC	FEP
	PSO							fi	1.05E=15	3.21E-18	1.05E-15	2.61E-12	3.21E-18	2.61E-12
fl	1.47E =0100	1.44E =01(0)	5.21E =03(1)	4.25E	1.21E -02(1)	6.08E	1.30E =01(0)	f2	(1) 2.61E-12	(1) 3.21E=18	(1) 2.33E-09	(1) 3.21E-18	(1) 2.16E=13	(1) 1.48E-07
f2	5.14E -02(0)	1.02E -01(0)	2.20E -01(0)	9.89E -03(1)	3.61E -02(1)	2.98E -02(1)	1.99E -03(1)	f3	(1) 1.12E-08	(1) 4.89E=03	(1) 2.33E-09	(1) 1.05E-15	(1) 1.05E=15	(1) 5.11E=02
-									(1)	(1)	(1)	(1)	(1)	(0)

6.34E 1.15E 2.34E 2.12E 7.55E 3.19E 1.26E 13 3.21E-18 1.56E-06 1.66E-17 6.14E-17 3.21E-18 14 3.21E-18 -02(0)-01(0)-02(1)-01(0)-02(0)-01(0)-02(1)(1) (1) (1) (1) (1) 9.35E 3.29E 2.92E 5.68E 6.21E 8.81E 5.27E 14 2.61E-12 15 4.22E-07 1.05E-1 2.61E-12 3.01E-14 1.23E-12 -02(0)-02(1)-04(1)-02(0)-03(1)-03(1)-02(0)(1) (1) (1) (1)(1) 15 4.96E 7.56E 4.53E 7.74E 5.78E 1.36E 9.98E 1.498-15 16 1.58E-12 1.59E-14 7.58E-09 3.21E-18 3.21E-18 -02(0)-02(0)-02(1)-02(0)-02(0)-01(0)-03(1)(iii) * (1) (1) (1) (1) (1) 7.81E 8.75E 1.95E 1.11E 2.69E 9.52E 16 9.60E 1.48E-1 3.21E-18 2.61E-12 3.11E-17 2.82E-11 6.14E-17 17 -02(0)-03(1)-02(1)-01(0)-02(1)-03(1)-02(0)2 (1) (1) (1) (1) (1) 17 5.66E 3.85E 5.44E 5.72E 1.11E 1.12E 1.58E 5.15E-01 4.58E-01 f8 6.85E-01 4.55E-01 5.16E-01 -03(1)-03(1)-03(1)-04(1)-01(0)-03(1)-02(1)(0) (0) (0)(0)(0) 8.11E 5.98E 5.23E 2.41E 1.36E 7.87E 1.54E 18 72NE-15 2.71E-10 2.33E-09 7.58E-09 6.14E-17 3.21E-18 19 -02(0)-02(0)-02(0)-01(0)-01(0)-02(0)-01(0)(1) (1) (1) (1) (1) (1) 4.48E 2.29E 19 4.14E 8.77E 6.45E 2.74E 4.72E CLO 6.14E-17 2.16E-13 2.61E-12 6.14E-17 4.46E-15 2.33E-09 -02(1)-02(0)-02(1)-02(0)-03(1)-02(1)-03(1)(1) (1) (1)(1) 5.07E (1)(1) 2.98E 5.67E f10 1.49E 1.89E 2.90E 4.29E -04(1) f11 4.54E-01 7.55E-01 8.42E-01 2.58E-01 9.48E-02 4.84E-01 -03(1)-02(1)-03(1)-01(0)-01(0)-02(1)٠ 1.55¥ (0) (0)(0) (0) fll 1.74E 7.41E 5.44E 7.44E 7.44E 1.44E (0)(0) -01(0)-02(0)-02(0)-02(0)-02(0)-01(0)f12 6.18E-01 6.09E-01 8.64E-01 1.25E-01 8.64E-01 8.64E-01 f12 3.47E 1.74E 6.11E 5.11E 1.41E 1.69E (0)(0) (0)(0) (0) (0) -06(1) -02(1-01(0)-01(0)-02(0)-02(0)-01(0)f13 8.64E-01 3.93E-01 6.09E-01 8.64E-01 2.16E-13 6.09E-01 4.738 6.77E 6.45E 1.92E f13 1.11E 4.08E 7.44E (0)(0) (0)(0) (1)(0) -02(0)-01(0)-04(1)-02(0)-02(0)-03(1)1.82E-01 6.33E-02 8.62E-03 8.80E-01 2.65E - 02f14 1.21E-01 CLERE 10(1) f14 7.44E 5.93E 5.83E 1.18E 7.06E 2.30E (0)(0) (1) (0) (1)(0) -02(0) -02(0)-02(1)-02(0)-01(0)-04(1)1.21E-1 f15 2.32E-01 1.850E-01 2.33E-01 2.32E-01 1.84E-01 1.25E 8.77E 7.58E f15 2.14E 4.14E 7.89E 1.24E (0)(0) (0)(1)(1)-01(0)-02(0)-14(1)-01(0)-02(0)-01(0)6.09E-01 f16 1.07E-01 1.72E-01 4.95E-01 1.18E-03 8.64E-01 f16 4.14E 4.55E 1.55E 5.44E 9.09E 9.08E (0) (0)(0) (1) (0) (0)-02(2) -01(0)-05(1)-01(0)-02(0)-03(1)-02(0)f173.21E-18 6.14E-17 3.21E-18 1.59E-14 3.21E-18 1.59E-14 1.062 f17 7.41E 2.19E 3.06E 2.56E 2.21E 6.90E (1)(1) (1)(1) (1) (1) -02(0)-03(1)-01(0)-02(1)-02(1)-03(1)f18 7.58E-09 3.21E-18 3.21E-18 2.61E-12 2.61E-12 1.05E-15 C-2.65E 1.28E 7.44E f18 8.03E 4.57E 6.55E 2.35E (1)(1)(1)(1) (1)(1) -01(0) 593E 1 -02(0)-03(1)-03(1)-02(0)-03(1)-03(1)2.71E-10 3.21E-18 f19 1.59E-14 2.16E-13 3.21E-18 6.14E-17 f19 7.71E 1.15E 8.70E 1.07E 1.56E 2.48E (1) (1) (1) (1) (1) (1) -39(1) 5.00E

f27 (0)

f20

f21

f22

f26

2.68E-03

1.57E-12

2.16E-13

5.49E-01

6.47E-01

(1)

(1)

(1)

(0)

4.64E-08

7.48E-14

1.78E-08

1.31E-04

2.04E-02

00

(1)

(1)

(1)

(1)

3.21E-18

4.45E-14

3.21E-18

2.37E-05

3.58E-05

(1)

(1)

(1)

(1)

(1)

4.14E-05

2.98E-09

3.21E-18

1.81E-05

3.21E-18

(1)

(1)

(1)

(1)

(1)

1.05E-14

5.55E-14

2.82E-11

6.72E-07

2.84E-02

(1)

(1)

(1)

(1)

(1)

3.21E-18

1.05E-15

1.59E-14

3.70E-08

1.71E-15

(1)

(1)

(1)

(1)

(1)

-02(0)

-03(1)

-01(0)

-02(0)

-02(0)

-02(1)

1.67E

f20 3.73E

f21 1.14E

f22 8.14E

f26 8.46E

127

-02(1)

4.17E

-02(1)

5.49E

-03(1)

1.24E

-03(1)

2.57E

-02(1)

7.88E

-02(0)

-02(0)

8.38E

-03(1)

3.99E

-02(1)

1.99E

-01(0)

3.39E

-02(1)

1.80E

-02(1)

-03(1)

6.82E

9.95E

-03(1)

2.97E

-02(1)

2.62E

-02(1)

-03(1)

-03(1)

4.73E

-02(1)

7.12E

-03(1)

5.86E

-02(0)

3.01E

-01(0)

2.34E

-04(1)

-01(0)

2.89E

-02(1)

2.46E

-01(0)

5.47E

-02(0)

1.90E

-02(0)

1.52E

-02(1)

-04(1)

2.01E

-02(1)

3.43E

-02(1)

8.13E

-04(1)

2.28E

-02(1)

4.05E

-02(1)



Comparison with Latest Best Algorithms

	TSC = PSO Mean	St. D	L = SHADE Mean	St. D	CETMS Mean	St. D	FWA = DM Mean	St. D
fl	1.38E+05	4.20E+04	1.70E+05	5.70E+04	0.00E+00	0.00E+00	2.28E+08	4.08E+07
f2	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1.62E+04	1.81E+04
f3	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	2.95E+04	3.64E+03
f4	2.21E+02	3.30E+01	1.70E+02	3.10E+01	7.13E+01	4.43E+01	1.83E+02	1.00E+02
f5	2.00E+01	1.20E-06	2.10E+01	3.10E-02	2301E+01	3.35E-01	2.10E+01	2.44E-02
f6	5.12E+00	1.65E+00	8.70E+00	2.30E+00	4.23E+00	2.60E+00	1.14E+02	2.54E+00
£7	0.00E+00	0.00E+00	0.00E+00	0.00E+00	4.59E-01	1.99E+00	1.29E-01	3.14E-02
fB	0.00E+00	0.00E+00	1.10E-02	7.40E-03	2.53E+01	5.52E+00	1.08E4-02	5.40E+00
f9	5.76E+01	2.56E+00	3.40E+01	5.00E+00	2.45E+01	8.14E+00	5.52E+02	4.44E+01
f10	4.22E+01	1.12E+01	2.60E+01	5.80E 90	3.91E+03	1.26E+03	5.67E+03	3.04E+02
f11	2.12E+04	1.32E+03	1.10E+04	5.602+82	4.29E+03	1.58E+03	1.46E4-04	6.30E+02
f12	1.96E-02	3.22E-03	4.40E-01	4708-02	1.51E-03	1.10E-03	1.21E+00	7.78E-02
f13	4.23E-01	2.45E-02	2.40E-01	2.10E-02	1.11E-01	4.21E-02	5.61E-01	3.61E-02
f14	2.66E-01	1.23E-02	1.20E-01	7.30E-03	5.00E-01	6.68E-02	1.89E-01	2.06E-02
f15	1.45E+03	2.30E+02	1.60E+01	1.20E+00	1.00E+01	2.24E+01	8.74E+01	5.87E+00
f16	3.86E+01	2.63E-01	3.90E+01*	4.80E-01	2.28E+01	1.51E+00	4.35E+01	3.75E-01
f17	7.07E+03	1.59E+03	4.40E+02	7.10E+02	2.16E+03	5.40E+02	2.31E+07	5.63E+06
f18	4.14E+02	7.86E+01	2.20E 02	1.70E+01	2.65E+02	6.47E+01	5.68E+03	8.70E+03
f19	6.41E+01	1.21E-01	9.505+01	2.30E+00	1.21E+01	3.14E+00	6.34E+01	2.43E+00
f20	9.86E+01	3.35E+01	1.50 = 02	5.20E+01	3.51E+02	1.53E+02	6.93E+04	1.10E+04
f21	3.12E+03	6.54E+02	2 30E+03	5.30E+02	1.36E+03	4.22E+02	9.57E+06	2.31E+06
f22	8.77E+02	1.54E+02	+1.10E+03	1.90E+02	3.68E+02	1.90E+02	1.51E+03	1.34E+02
f23	3.00E+02	6.40E-11	3.50E+02	2.80E-13	3.44E+02	2.87E-13	3.46E+02	2.18E-01
f24	3.05E+02	4.12E+60	3.90E+02	2.90E+00	2.75E+02	1.14E+00	3.63E+02	2.85E+00
f25	2.00E+02	3.40E-12	2.00E+02	4.00E-13	2.08E+02	2.77E+00	3.03E+02	1.74E+01
f26	1.06E+02	6.60E-13	2.00E+02	6.20E-13	1.75E+02	1.02E+02	1.61E+02	5.88E+0 I
f27	4.00E+02	2.20E-05	3.80E+02	3.30E+01	4.54E+02	7.34E+01	3.14E+03	4.13E+02
f28	3.00E+02	4.51E-05	2.30E+03	4.60E+01	1.27E+03	8.63E+01	1.60E+03	3.42E+02
f29	7.33E+02	1.21E+01	8.00E+02	7.60E+01	2.26E+06	9.16E+06	2.70E+02	5.23E+00
f30	2.12E+03	5.46E+02	8.30E+03	9.60E+02	9.81E+03	1.73E+03	2.23E+03	1.16E+03



SW and Wilcoxon Test



-				-	~O'	•	
	<i>TSC - PSO</i> SW: p (h)	L - SHADE SW: p (h)	W: p (h)	CETMS SW: p (h)	Wager	<i>FWA</i> - <i>DM</i> SW : p (h)	W: p (h)
fl	3.56E-03(1)	1.18E-02(1)	4.13E-03(1)	7.51E-02(0)	5.15E-07(1)	7.01E-02(0)	1.69E-06(1)
f2	8.77E-02(0)	1.27E-01(0)	1.51E-01(0)	6.14E-02(0)	8.80E-02(0)	2.31E-03(1)	7.45E-07(1)
f3	5.45E-02(0)	5.45E-02(0)	7.85E-01(0)	5.15E-02(0)	1.07E-01(0)	5.36E-03(1)	3.77E-07(1)
f4	4.60E-02(1)	7.47E-03(1)	1.15E-09(1)	8.19E-03(2)	2.39E-06(1)	4.20E-03(1)	1.40E-01(0)
f5	1.18E-06(1)	2.85E-03(1)	1.88E-06(1)	2.48E-03(1)	1.05E-02(1)	1.55E-03(1)	2.78E-06(1)
f6	5.57E-02(0)	1.39E-02(1)	1.08E-10(1)	1.82E-64(0)	5.96E-02(0)	4.47E-02(1)	2.80E-06(1)
f7	7.44E-02(0)	7.12E-02(0)	8.78E-02(0)	1.39E-02(1)	2.65E-02(1)	1.20E-02(1)	2.55E-06(1)
fB	5.12E-02(0)	2.03E-02(1)	2.16E-13(1)	1.16E-02(1)	1.34E-07(1)	4.09E-02(1)	2.75E-07(1)
f9	1.40E-02(1)	2.42E-01(0)	1.28E-06(1)	1.95E-02(1)	2.12E-06(1)	3.55E-03(1)	2.62E-06(1)
f10	9.15E-04(1)	2.62E-03(1)	3.64E-12(1)	6.34E-02(0)	1.63E-06(1)	2.21E-02(1)	3.28E-06(1)
f11	5.07E-03(1)	1.84E-02(1)	2.87E-06(1)	5.71E-02(0)	3.87E-06(1)	8.45E-03(1)	2.13E-06(1)
f12	4.82E-02(1)	1.79E-02(1)	1.30E-06(f)	7.07E-03(1)	4.23E-07(1)	6.09E-02(0)	2.44E-06(1)
f13	2.73E-03(1)	8.52E-03(1)	3.12E-66	4.24E-03(1)	1.69E-06(1)	2.65E-02(1)	3.63E-07(1)
f14	2.05E-02(1)	1.56E-02(1)	1.07(-96(1)	4.04E-03(1)	6.15E-07(1)	1.76E-01(0)	1.12E-06(1)
f15	2.13E-01(0)	8.12E-03(1)	1-765-06(1)	4.68E-02(1)	2.11E-06(1)	1.23E-02(1)	1.83E-06(1)
f16	1.32E-01(0)	4.75E-03(1)	522E-05(1)	2.24E-02(1)	3.50E-06(1)	2.58E-03(1)	2.07E-06(1)
f17	4.39E-02(1)	1.14E-02(1)	2.77E-15(1)	2.18E-02(1)	3.77E-06(1)	4.76E-02(1)	2.55E-06(1)
f18	1.09E-02(1)	3.30E-03(1)	3.83E-06(1)	1.65E-02(1)	4.33E-13(1)	1.16E-01(0)	8.66E-05(1)
f19	4.66E-03(1)	7.57E-04(1)	9.63E-07(1)	1.50E-02(1)	2.70E-06(1)	7.52E-02(0)	3.37E-01(0)
f20	1.26E-02(1)	1.16E-02	1.28E-06(1)	2.28E-02(1)	6.51E-15(1)	2.42E-03(1)	1.16E-06(1)
f21	2.56E-02(1)	4.76E-02(1)	3.70E-08(1)	1.70E-02(1)	2.69E-06(1)	6.63E-04(1)	2.78E-06(1)
f22	1.03E-02(1)	2.29E-03(1)	1.31E-07(1)	1.46E-03(1)	9.76E-18(1)	4.12E-04(1)	2.72E-07(1)
f23	1.22E-01(0)	5 BNE-02(0)	1.02E-06(1)	1.71E-01(0)	8.96E-07(1)	1.07E-02(1)	2.67E-06(1)
f24	2.47E-02(1)	1.T3E-03(1)	3.38E-06(1)	1.87E-02(1)	1.38E-06(1)	6.28E-02(0)	3.12E-06(1)
f25	5.43E-02(0)	2.11E-01(0)	8.15E-01(0)	2.10E-02(1)	2.70E-06(1)	2.50E-03(1)	2.69E-08(1)
f26	1.44E-01(0)	1.24E-01(1)	2.41E-06(1)	5.16E-03(1)	8.66E-05(1)	1.24E-01(0)	7.45E-07(1)
f27	9.46E-07(1)	7.14E-03(1)	3.72E-03(1)	4.75E-03(1)	8.66E-05(1)	7.30E-03(1)	1.55E-06(1)
f28	2.18E-05(1)	1.59E-01(0)	3.66E-06(1)	1.69E-02(1)	4.60E-09(1)	9.52E-02(0)	1.85E-06(1)
f29	5.03E-03(1)	4.69E-02(1)	5.78E-06(1)	2.42E-01(0)	2.32E-01(0)	3.47E-02(1)	1.70E-06(1)
f30	9.84E-04(1)	1.14E-01(0)	1.84E-06(1)	1.21E-02(1)	3.08E-06(1)	3.19E-03(1)	6.42E-01(0)



